

Appendix E-1

Tamarisk Apartment Complex, Hesperia

APN: 3057-121-08

Preliminary Drainage Report

Allard Engineering

May 6, 2024



ALLARD ENGINEERING

civil engineering land surveying land planning

Tamarisk Apartment Complex, Hesperia

APN: 3057-121-08

Preliminary Drainage Report

May 6, 2024

Prepared For:

Munem Maida

13302 Ranchero Road

Hesperia, CA 92344

Tel:

Prepared By:

Allard Engineering

16866 Seville Ave

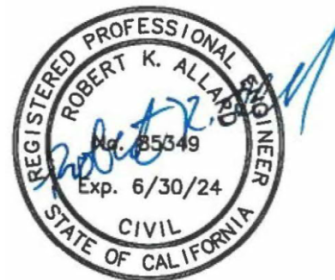
Fontana, CA 92335

Tel: (909) 356-1815

Email: rallard@allardeng.com

Prepared under the supervision of:

Robert K. Allard



Bobby K Allard, P.E. RCE 85349 Exp. 03-11-2024

Discussion

Introduction

The proposed 4.9 acres of the proposed apartment complex development in the City of Hesperia, County of San Bernardino. The proposed apartment complex development area lies south of Main Street, west of Tamarisk Road, and east of Topaz Avenue.

The site is located within the City of Hesperia Master Plan of Drainage System (Proposed Regional Facility Line H-04-01) which will be built by the City of Hesperia in future. The entire site will drain to the proposed two below surface Stormtech infiltration/retention chamber system at the site. The proposed retention/infiltration chamber systems are sized to qualify for both WQMP volume as well as the retention volume from the site. The proposed infiltration/retention chamber systems will drain out to the existing street gutter in the Tamarisk Road on surface once they reach the capacity and keep draining on Tamarisk Road then to the east into the Main Street.

There are no offsite runoff from upstream tributary areas to the site. Offsite runoff intercepted north of the site by Main Street.

Purpose

The purpose of this Drainage Report is to determine storm water runoff for onsite. Also to show that the proposed retention/infiltration chamber systems are adequately sized to convey the onsite runoff (upto 100-yr storm event) in a safe manner to the existing street gutter in Tamarisk Avenue. Detailed hydrology analysis and calculations are provided with this report for the onsite developed condition and existing condition.

Criteria

The criteria utilized for hydrologic analysis is the San Bernardino County Hydrology Manual, AES rational method hydrology analysis and the City of Hesperia Master Plan of Drainage. AES software (Rational Method Hydrology) was used to quantify onsite runoff and "13.5-cf of retention per 100-sf of impervious area" rule was used to quantify onsite detention volume. AES software were used for the proposed storm drain system onsite.

Findings

The proposed site development (4.9 acres, apartment complex) (APN: 3057-121-08) and its drainage system will comprise of storm drain pipe, ribbon/valley gutters onsite drop/grate inlets with filtration device, and multiple infiltration/retention chamber system. The infiltration/retention chamber system-1,2 are sized to qualify for both WQMP volume as well as the detention volume for the proposed developed site. Detention volume has been calculated based upon the City of Hesperia "13.5-cf of retention per 100-sf of impervious area" rule.

We calculated the runoff quantities of 18.6 cfs onsite in developed condition and 12.9 cfs in pre-developed condition using the rational method hydrology analysis for the 100-yr storm event.

The onsite runoff of 18.6 cfs generated from the proposed site in developed condition which is 4.90 acres. The onsite runoff (18.6 cfs) will be drained into the proposed two below surface infiltration/retention chamber system-1,2 for WQ volume (16,314 CF) infiltration and retention/infiltration (25,933 CF) of the

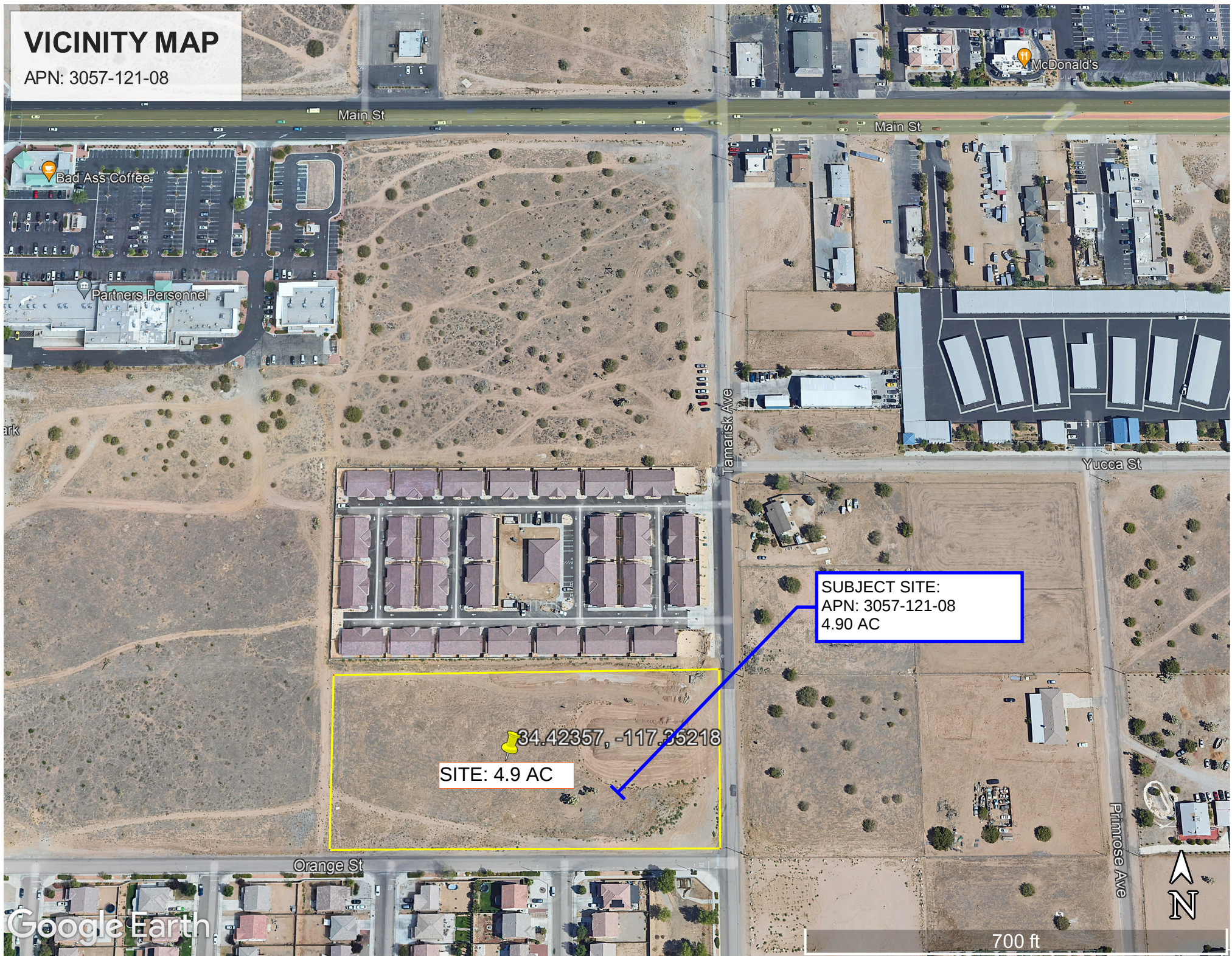
City required detention volume to mitigate HCOC condition. Once all of the retention/infiltration chamber system-1,2 reach their capacity, it will drain out to street gutter in Tamarisk Avenue at the east boundary line of the site. The runoff will follow the existing drainage course on Tamarisk Avenue and ultimately drain to the Mojave River which is the receiving water.

Reference plans/documents, calculations and the exhibits are attached to support these findings.

Reference Material

VICINITY MAP

APN: 3057-121-08





POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin,
Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao,
Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerals](#)

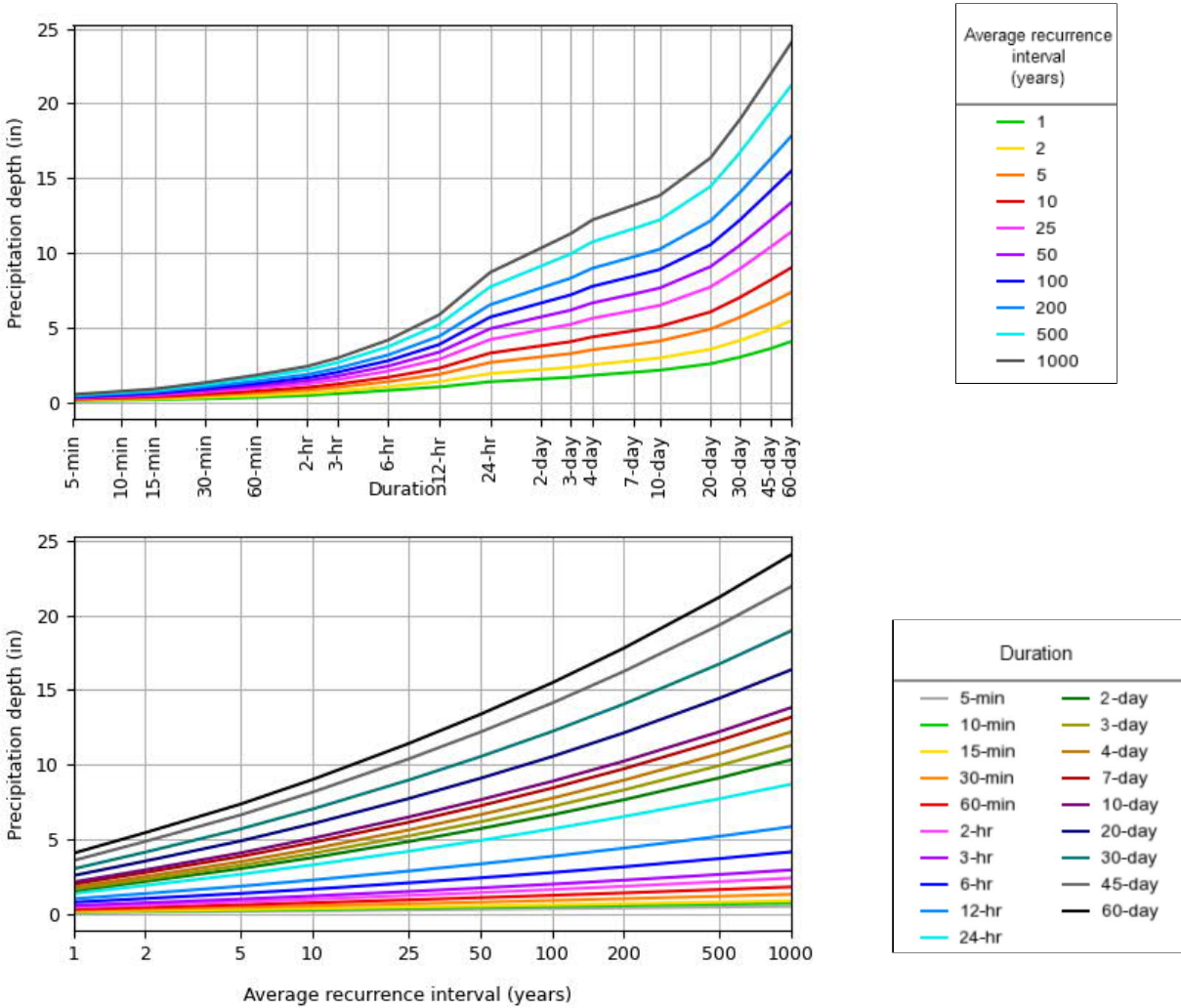
PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.085 (0.071-0.104)	0.121 (0.100-0.147)	0.168 (0.138-0.205)	0.206 (0.169-0.255)	0.260 (0.205-0.332)	0.302 (0.234-0.394)	0.345 (0.261-0.462)	0.390 (0.287-0.537)	0.453 (0.319-0.650)	0.502 (0.342-0.746)
10-min	0.122 (0.101-0.149)	0.173 (0.143-0.211)	0.240 (0.198-0.294)	0.296 (0.242-0.365)	0.373 (0.295-0.476)	0.433 (0.335-0.565)	0.495 (0.374-0.662)	0.560 (0.411-0.770)	0.649 (0.457-0.931)	0.720 (0.490-1.07)
15-min	0.148 (0.122-0.180)	0.209 (0.173-0.256)	0.290 (0.239-0.356)	0.358 (0.292-0.442)	0.451 (0.356-0.576)	0.523 (0.405-0.683)	0.598 (0.452-0.800)	0.677 (0.497-0.931)	0.785 (0.553-1.13)	0.871 (0.593-1.29)
30-min	0.221 (0.183-0.270)	0.313 (0.258-0.382)	0.434 (0.358-0.532)	0.535 (0.437-0.661)	0.674 (0.533-0.861)	0.782 (0.606-1.02)	0.895 (0.676-1.20)	1.01 (0.743-1.39)	1.17 (0.827-1.68)	1.30 (0.886-1.93)
60-min	0.306 (0.253-0.373)	0.432 (0.357-0.528)	0.601 (0.495-0.736)	0.740 (0.604-0.914)	0.932 (0.737-1.19)	1.08 (0.838-1.41)	1.24 (0.935-1.66)	1.40 (1.03-1.92)	1.62 (1.14-2.33)	1.80 (1.23-2.67)
2-hr	0.442 (0.365-0.539)	0.596 (0.492-0.728)	0.804 (0.663-0.986)	0.979 (0.801-1.21)	1.22 (0.969-1.57)	1.42 (1.10-1.86)	1.63 (1.23-2.17)	1.84 (1.35-2.53)	2.15 (1.51-3.08)	2.39 (1.63-3.54)
3-hr	0.554 (0.459-0.677)	0.737 (0.609-0.900)	0.985 (0.812-1.21)	1.20 (0.977-1.48)	1.49 (1.18-1.91)	1.73 (1.34-2.26)	1.98 (1.50-2.65)	2.25 (1.65-3.10)	2.63 (1.85-3.77)	2.94 (2.00-4.36)
6-hr	0.777 (0.643-0.949)	1.02 (0.846-1.25)	1.36 (1.12-1.67)	1.65 (1.35-2.04)	2.07 (1.64-2.64)	2.40 (1.86-3.14)	2.76 (2.08-3.69)	3.15 (2.31-4.33)	3.70 (2.60-5.30)	4.15 (2.82-6.16)
12-hr	1.00 (0.829-1.22)	1.36 (1.12-1.66)	1.84 (1.52-2.26)	2.26 (1.85-2.79)	2.86 (2.26-3.65)	3.34 (2.58-4.35)	3.85 (2.91-5.14)	4.40 (3.23-6.05)	5.19 (3.65-7.44)	5.83 (3.97-8.66)
24-hr	1.36 (1.20-1.56)	1.90 (1.68-2.19)	2.64 (2.33-3.05)	3.28 (2.87-3.82)	4.18 (3.54-5.03)	4.91 (4.07-6.03)	5.68 (4.60-7.15)	6.51 (5.13-8.44)	7.70 (5.82-10.4)	8.68 (6.34-12.1)
2-day	1.54 (1.37-1.78)	2.16 (1.92-2.49)	3.02 (2.67-3.49)	3.76 (3.29-4.38)	4.83 (4.09-5.81)	5.70 (4.73-7.00)	6.63 (5.37-8.35)	7.64 (6.02-9.89)	9.10 (6.88-12.3)	10.3 (7.53-14.4)
3-day	1.65 (1.47-1.90)	2.32 (2.05-2.67)	3.24 (2.86-3.75)	4.04 (3.54-4.71)	5.20 (4.41-6.26)	6.15 (5.11-7.57)	7.18 (5.82-9.04)	8.30 (6.54-10.7)	9.92 (7.50-13.4)	11.3 (8.24-15.8)
4-day	1.78 (1.58-2.05)	2.50 (2.21-2.88)	3.49 (3.08-4.03)	4.35 (3.81-5.07)	5.60 (4.75-6.74)	6.63 (5.50-8.15)	7.74 (6.27-9.75)	8.95 (7.05-11.6)	10.7 (8.10-14.5)	12.2 (8.90-17.0)
7-day	1.99 (1.76-2.29)	2.76 (2.44-3.18)	3.84 (3.39-4.44)	4.77 (4.18-5.56)	6.12 (5.18-7.37)	7.22 (6.00-8.88)	8.42 (6.82-10.6)	9.72 (7.65-12.6)	11.6 (8.77-15.7)	13.2 (9.62-18.4)
10-day	2.12 (1.88-2.45)	2.94 (2.61-3.39)	4.08 (3.60-4.71)	5.06 (4.43-5.89)	6.47 (5.48-7.79)	7.63 (6.33-9.38)	8.87 (7.19-11.2)	10.2 (8.06-13.2)	12.2 (9.22-16.5)	13.8 (10.1-19.3)
20-day	2.56 (2.27-2.94)	3.53 (3.12-4.07)	4.88 (4.30-5.63)	6.03 (5.28-7.03)	7.70 (6.52-9.27)	9.06 (7.52-11.1)	10.5 (8.53-13.3)	12.1 (9.55-15.7)	14.4 (10.9-19.5)	16.3 (11.9-22.8)
30-day	3.01 (2.66-3.46)	4.13 (3.66-4.76)	5.68 (5.02-6.56)	7.02 (6.14-8.17)	8.94 (7.58-10.8)	10.5 (8.73-12.9)	12.2 (9.89-15.4)	14.1 (11.1-18.2)	16.7 (12.6-22.6)	19.0 (13.8-26.5)
45-day	3.56 (3.16-4.10)	4.84 (4.29-5.58)	6.62 (5.84-7.65)	8.15 (7.14-9.49)	10.4 (8.77-12.5)	12.2 (10.1-15.0)	14.1 (11.4-17.8)	16.2 (12.8-21.0)	19.3 (14.6-26.1)	21.9 (16.0-30.6)
60-day	4.05 (3.59-4.67)	5.43 (4.81-6.26)	7.35 (6.49-8.49)	9.00 (7.88-10.5)	11.4 (9.65-13.7)	13.3 (11.1-16.4)	15.5 (12.5-19.5)	17.8 (14.0-23.1)	21.2 (16.0-28.6)	24.1 (17.6-33.6)
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at low er and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.										

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PF graphical

PDS-based depth-duration-frequency (DDF) curves
Latitude: 34.4236°, Longitude: -117.3522°



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Maps & aerals

Small scale terrain

San Bernardino County, California, Mojave River Area

134—HESPERIA LOAMY FINE SAND, 2 TO 5 PERCENT SLOPES

Map Unit Setting

National map unit symbol: hks7

Elevation: 200 to 4,000 feet

Mean annual precipitation: 6 to 9 inches

Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 150 to 250 days

Farmland classification: Prime farmland if irrigated

Map Unit Composition

Hesperia and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hesperia

Setting

Landform: Fan aprons

Landform position (two-dimensional): Footslope

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Alluvium derived from granite sources

Typical profile

H1 - 0 to 6 inches: loamy fine sand

H2 - 6 to 60 inches: sandy loam

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High
(1.98 to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Avg: 3.96"/hr

Calcium carbonate, maximum content: 10 percent

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 5.9 inches)

Interpretive groups

Land capability classification (irrigated): 2e

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: R030XE006CA - COARSE LOAMY

Hydric soil rating: No

Minor Components

Wrightwood

Percent of map unit: 5 percent

Hydric soil rating: No

Cajon

Percent of map unit: 5 percent

Hydric soil rating: No

Bull trail

Percent of map unit: 3 percent

Hydric soil rating: No

Unnamed soils

Percent of map unit: 2 percent

Hydric soil rating: No

Data Source Information

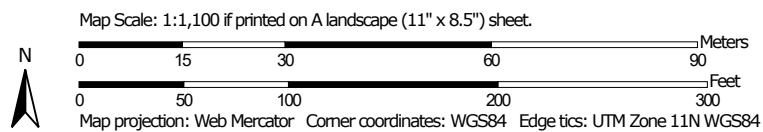
Soil Survey Area: San Bernardino County, California, Mojave River Area

Survey Area Data: Version 15, Aug 30, 2023

Soil Map—San Bernardino County, California, Mojave River Area



Soil Map may not be valid at this scale.



**Natural Resources
Conservation Service**

Web Soil Survey
National Cooperative Soil Survey

5/2/2024
Page 1 of 3

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: San Bernardino County, California, Mojave River Area

Survey Area Data: Version 15, Aug 30, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Mar 17, 2022—Jun 12, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
134	HESPERIA LOAMY FINE SAND, 2 TO 5 PERCENT SLOPES	4.2	100.0%
Totals for Area of Interest		4.2	100.0%

Worksheet H: Factor of Safety and Design Infiltration Rate and Worksheet

Factor Category		Factor Description	Assigned Weight (w)	Factor Value (v)	Product (p) p = w x v
A	Suitability Assessment	Soil assessment methods	0.25	2	0.50
		Predominant soil texture	0.25	2	0.50
		Site soil variability	0.25	1	0.25
		Depth to groundwater / impervious layer	0.25	1	0.25
		Suitability Assessment Safety Factor, S _A = Σp			
B	Design	Tributary area size	0.25	2	0.50
		Level of pretreatment/ expected sediment loads	0.25	2	0.50
		Redundancy	0.25	3	0.75
		Compaction during construction	0.25	1	0.25
		Design Safety Factor, S _B = Σp			
Combined Safety Factor, S _{TOT} = S _A x S _B				3.00	
Measured Infiltration Rate, inch/hr, K _M (corrected for test-specific bias)				3.96	
Design Infiltration Rate, in/hr, K _{DESIGN} = S _{TOT} / K _M				1.32	
Supporting Data					
Briefly describe infiltration test and provide reference to test forms:					
Average Inf. Rate : 3.96 in/hr from USDA WebSoil Report Design Inf Rate: 3.96/3.0 = 1.32"/hr					

Note: The minimum combined adjustment factor shall not be less than 2.0 and the maximum combined adjustment factor shall not exceed 9.0.

ACTUAL IMPERVIOUS COVER

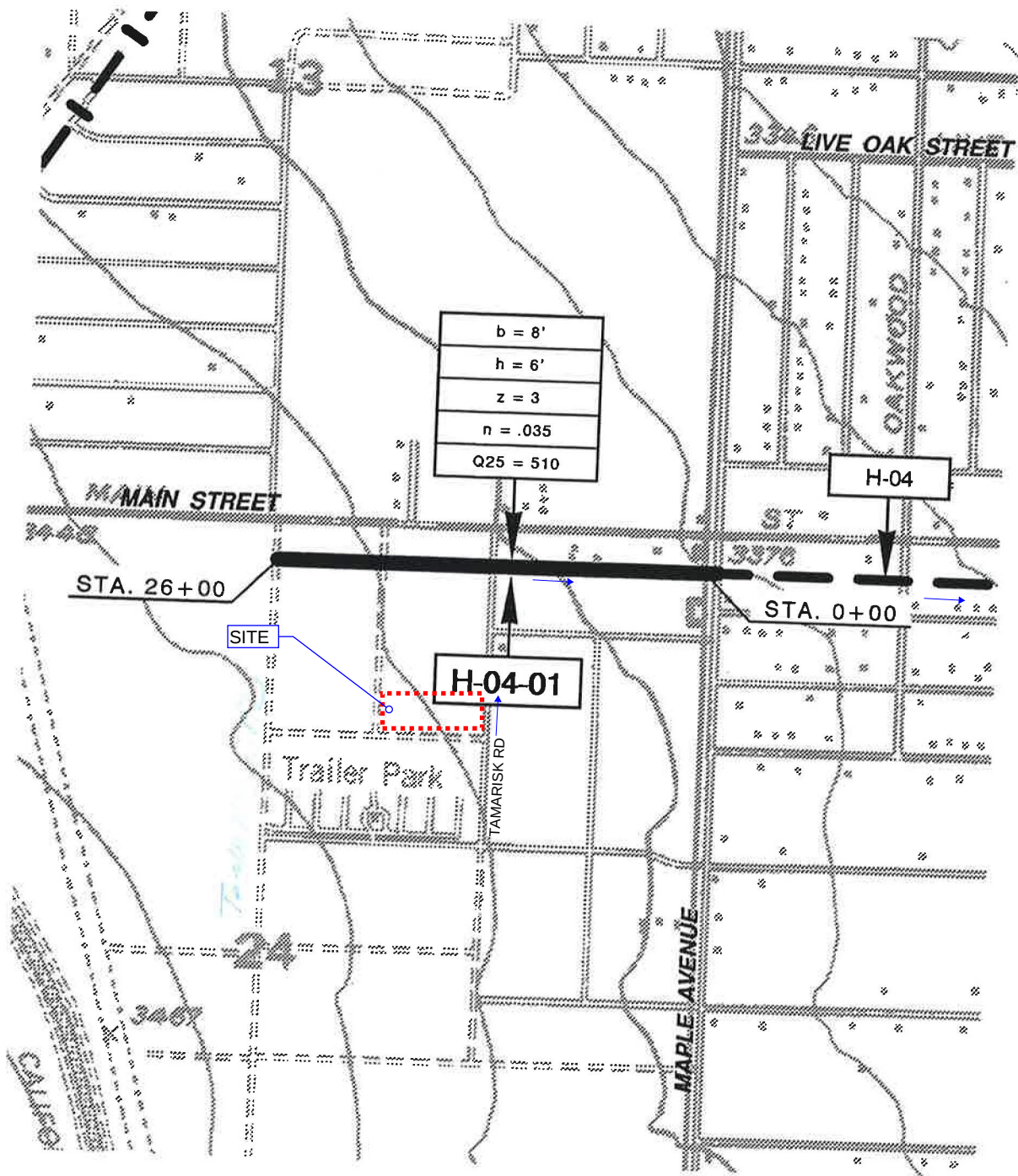
Land Use (1)	Range-Percent	Recommended Value For Average Conditions-Percent (2)
Natural or Agriculture	0 - 0	0
Public Park	10 - 25	15
School	30 - 50	40
Single Family Residential: (3)		
2.5 acre lots	5 - 15	10
1 acre lots	10 - 25	20
2 dwellings/acre	20 - 40	30
3-4 dwellings/acre	30 - 50	40
5-7 dwellings/acre	35 - 55	50
8-10 dwellings/acre	50 - 70	60
More than 10 dwellings/acre	65 - 90	80
Multiple Family Residential:		
Condominiums	45 - 70	65
Apartments	65 - 90	80
Mobile Home Park	60 - 85	75
Commercial, Downtown Business or Industrial	80 - 100	90

Notes:

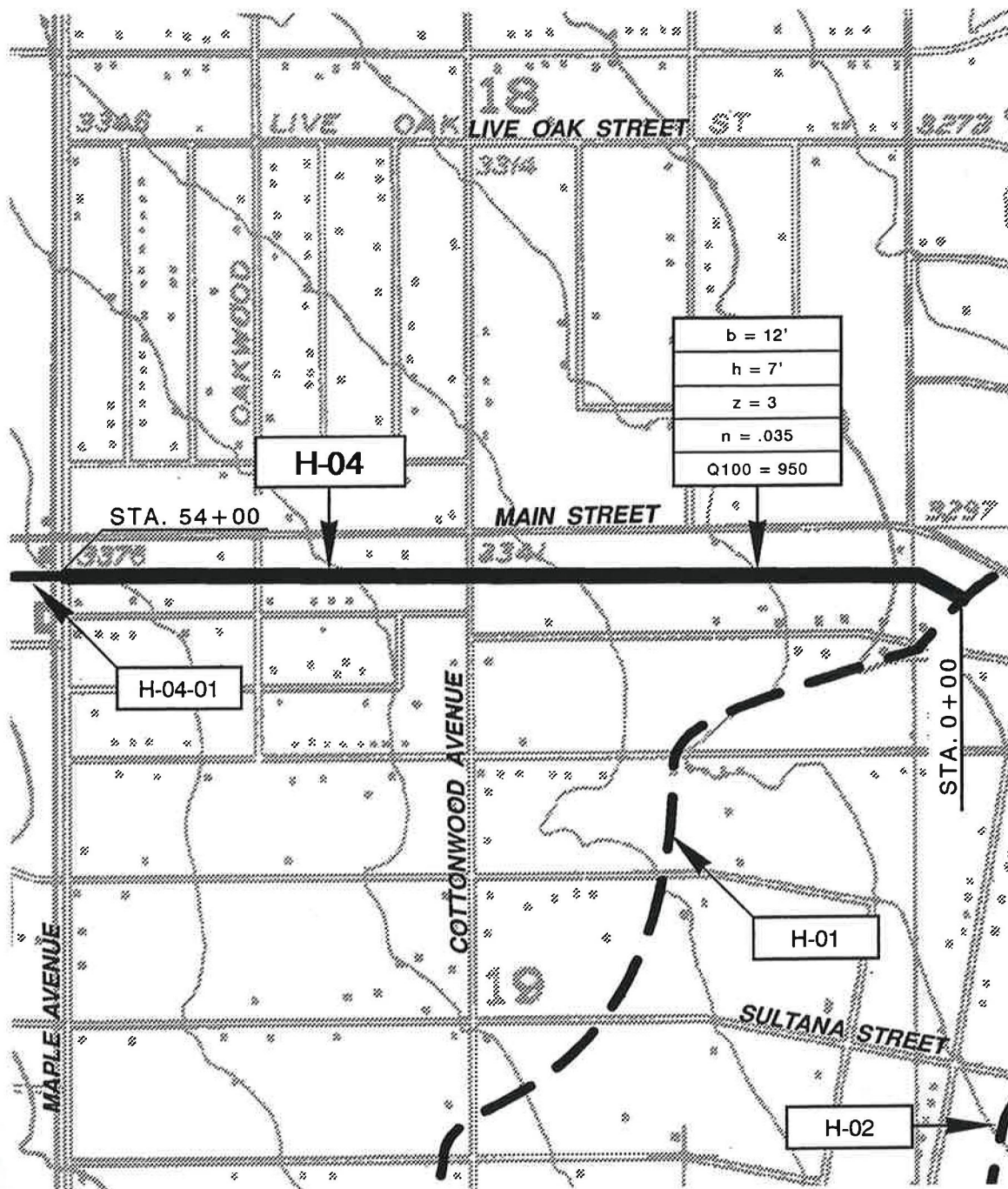
1. Land use should be based on ultimate development of the watershed. Long range master plans for the County and incorporated cities should be reviewed to insure reasonable land use assumptions.
2. Recommended values are based on average conditions which may not apply to a particular study area. The percentage impervious may vary greatly even on comparable sized lots due to differences in dwelling size, improvements, etc. Landscape practices should also be considered as it is common in some areas to use ornamental gravels underlain by impervious plastic materials in place of lawns and shrubs. A field investigation of a study area shall always be made, and a review of aerial photos, where available, may assist in estimating the percentage of impervious cover in developed areas.
3. For typical equestrian subdivisions increase impervious area 5 percent over the values recommended in the table above.

SAN BERNARDINO COUNTY
HYDROLOGY MANUAL

**ACTUAL IMPERVIOUS COVER
FOR
DEVELOPED AREAS**



LEGEND PROPOSED FACILITY FACILITY SHOWN ELSEWHERE WATERSHED BOUNDARY FLOODPLAIN FLOODWAY DETENTION BASIN	HESPERIA H-04-01 SHEET 1 OF 1		WILLIAMSON & SCHMID SCALE 1" = 1000'
	MASTER PLAN OF DRAINAGE		



LEGEND

- PROPOSED FACILITY
- FACILITY SHOWN ELSEWHERE
- WATERSHED BOUNDARY

- FLOODPLAIN
- FLOODWAY
- DETENTION BASIN

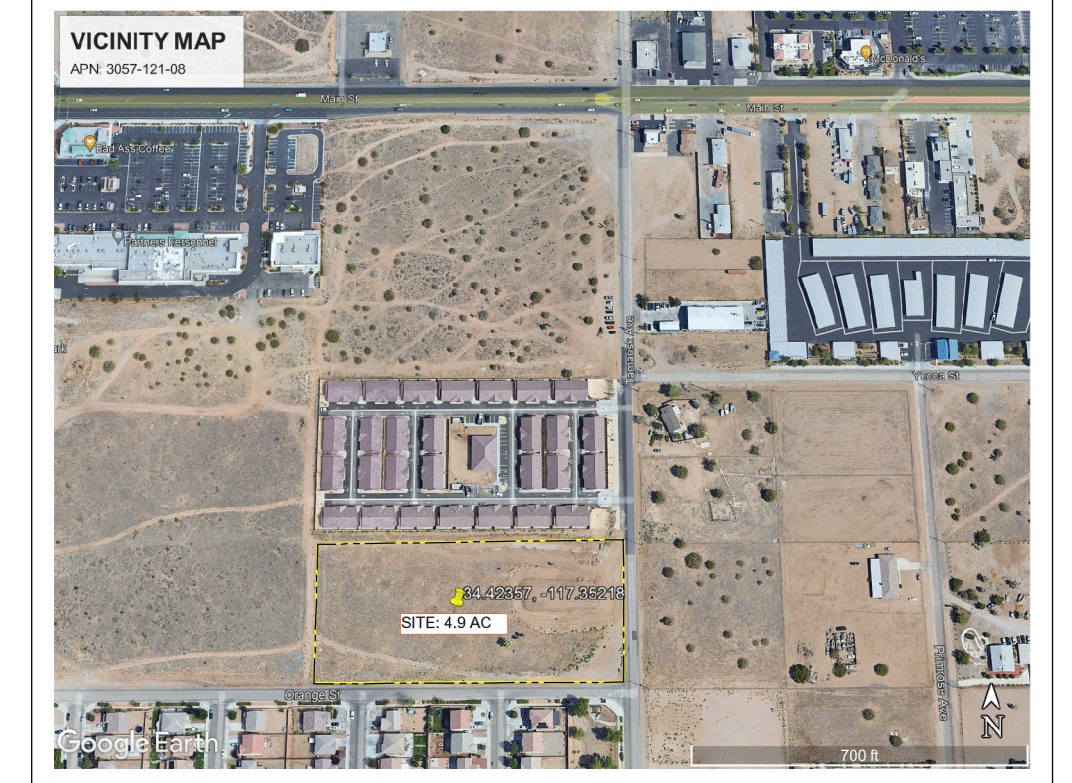
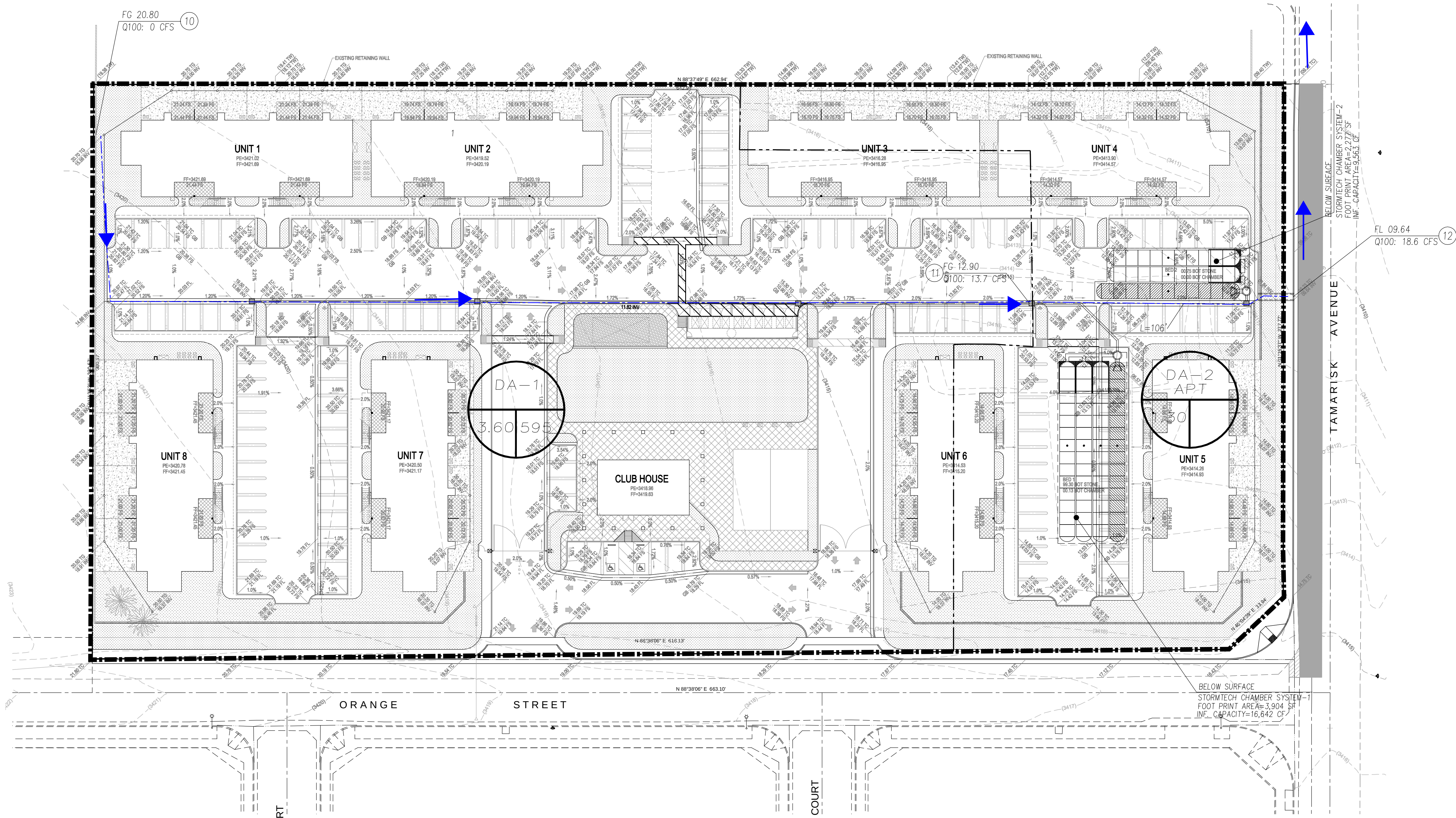
MASTER PLAN
OF
DRAINAGE

HESPERIA
H-04
SHEET 1 OF 1

WILLIAMSON & SCHMID
SCALE
1" = 1000'

**ONSITE RATIONAL METHOD
HYDROLOGY ANALYSIS (100-YR
STORM EVENT)**

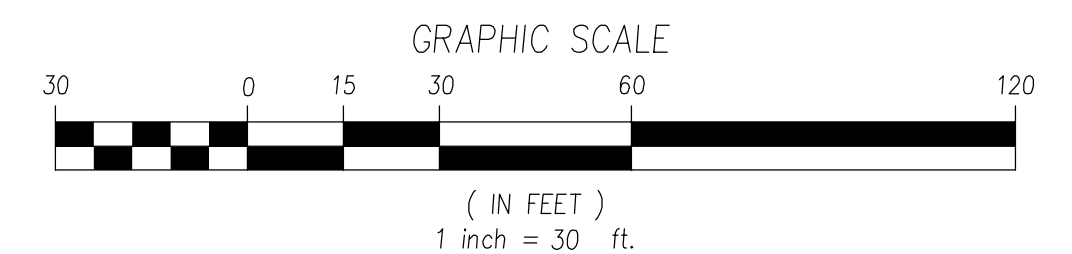
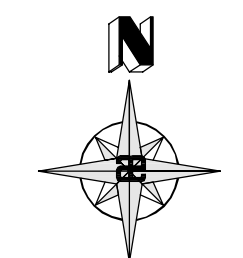
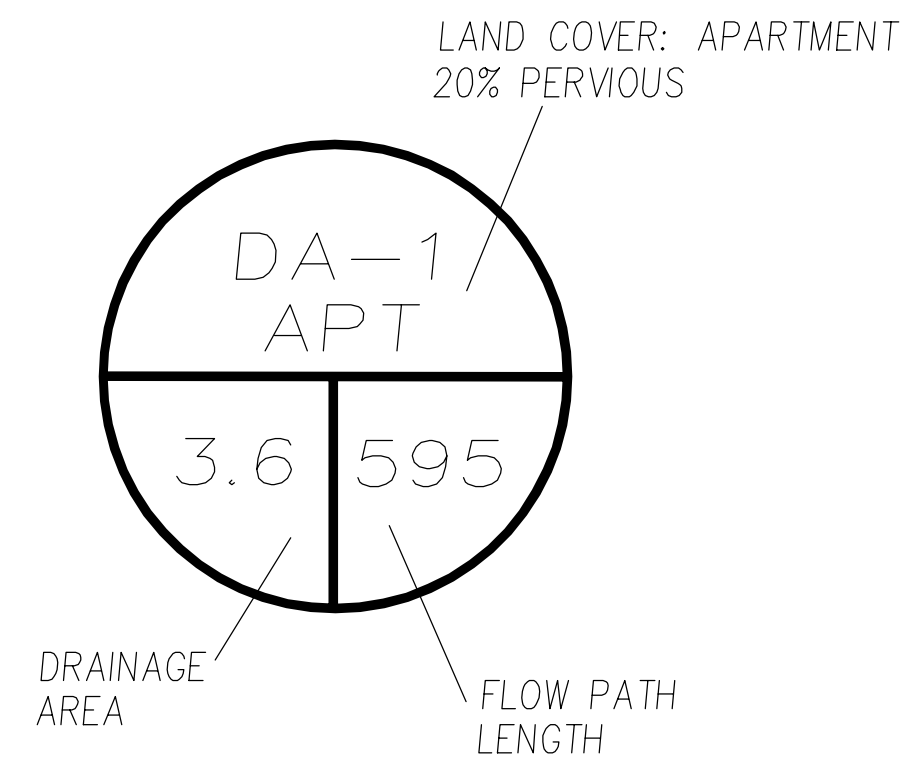
PLOT DATE: May 06, 2024, ashafiq



VICINITY MAP
NTS



LATITUDE & LONGITUDE
34.42357° N, -117.35218° W



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Prepared For:
MUNEM MAIDA
13302 RANCHERO ROAD
HESPERIA, CA92344

**CITY OF HESPERIA
CALIFORNIA**
DRAINAGE EXHIBIT
(DEVELOPED CONDITION)
TAMARISK AVENUE APT. COMPLEX-2
APN :3057-121-08

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)
(c) Copyright 1983-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1400

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* TAMARISK APARTMENT *
* HYDROLOGY ANALYSIS *
* 100YR STORM EVENT, DEVELOPED CONDITION *

FILE NAME: TAM.DAT
TIME/DATE OF STUDY: 15:22 05/06/2024

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 48.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL

SLOPE OF INTENSITY DURATION CURVE(LOG(I;IN/HR) vs. LOG(Tc;MIN)) = 0.7000
USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 1.2400

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	CROWN TO STREET-CROSSFALL:		CURB GUTTER-GEOMETRIES: MANNING	HEIGHT	WIDTH	LIP	HIKE	FACTOR
	WIDTH (FT)	CROSSFALL (FT)						
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 595.00
ELEVATION DATA: UPSTREAM(FEET) = 20.80 DOWNSTREAM(FEET) = 12.90

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.902
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.376
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	A	3.60	0.74	0.200	52	9.90

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 13.70

TOTAL AREA(ACRES) = 3.60 PEAK FLOW RATE(CFS) = 13.70

FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	12.90	DOWNSTREAM(FEET) =	9.64
CHANNEL LENGTH THRU SUBAREA(FEET) =	106.00	CHANNEL SLOPE =	0.0308
CHANNEL BASE(FEET) =	3.00	"Z" FACTOR =	18.000
MANNING'S FACTOR =	0.015	MAXIMUM DEPTH(FEET) =	0.08

==>>WARNING: FLOW IN CHANNEL EXCEEDS CHANNEL
CAPACITY(NORMAL DEPTH EQUAL TO SPECIFIED MAXIMUM
ALLOWABLE DEPTH).
AS AN APPROXIMATION, FLOWDEPTH IS SET AT MAXIMUM
ALLOWABLE DEPTH AND IS USED FOR TRAVELTIME CALCULATIONS.

* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.364
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
MOBILE HOME PARK	A	1.30	0.74	0.250	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.250
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.14
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 43.28
AVERAGE FLOW DEPTH(FEET) = 0.08 TRAVEL TIME(MIN.) = 0.04
Tc(MIN.) = 9.94

SUBAREA AREA(ACRES) =	1.30	SUBAREA RUNOFF(CFS) =	4.89
EFFECTIVE AREA(ACRES) =	4.90	AREA-AVERAGED Fm(INCH/HR) =	0.16
AREA-AVERAGED Fp(INCH/HR) =	0.74	AREA-AVERAGED Ap =	0.21
TOTAL AREA(ACRES) =	4.9	PEAK FLOW RATE(CFS) =	18.55

==>>WARNING: FLOW IN CHANNEL EXCEEDS CHANNEL
CAPACITY(NORMAL DEPTH EQUAL TO SPECIFIED MAXIMUM
ALLOWABLE DEPTH).
AS AN APPROXIMATION, FLOWDEPTH IS SET AT MAXIMUM
ALLOWABLE DEPTH AND IS USED FOR TRAVELTIME CALCULATIONS.

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 49.72

==>FLOWDEPTH EXCEEDS MAXIMUM ALLOWABLE DEPTH

LONGEST FLOWPATH FROM NODE 10.00 TO NODE 12.00 = 701.00 FEET.

=====

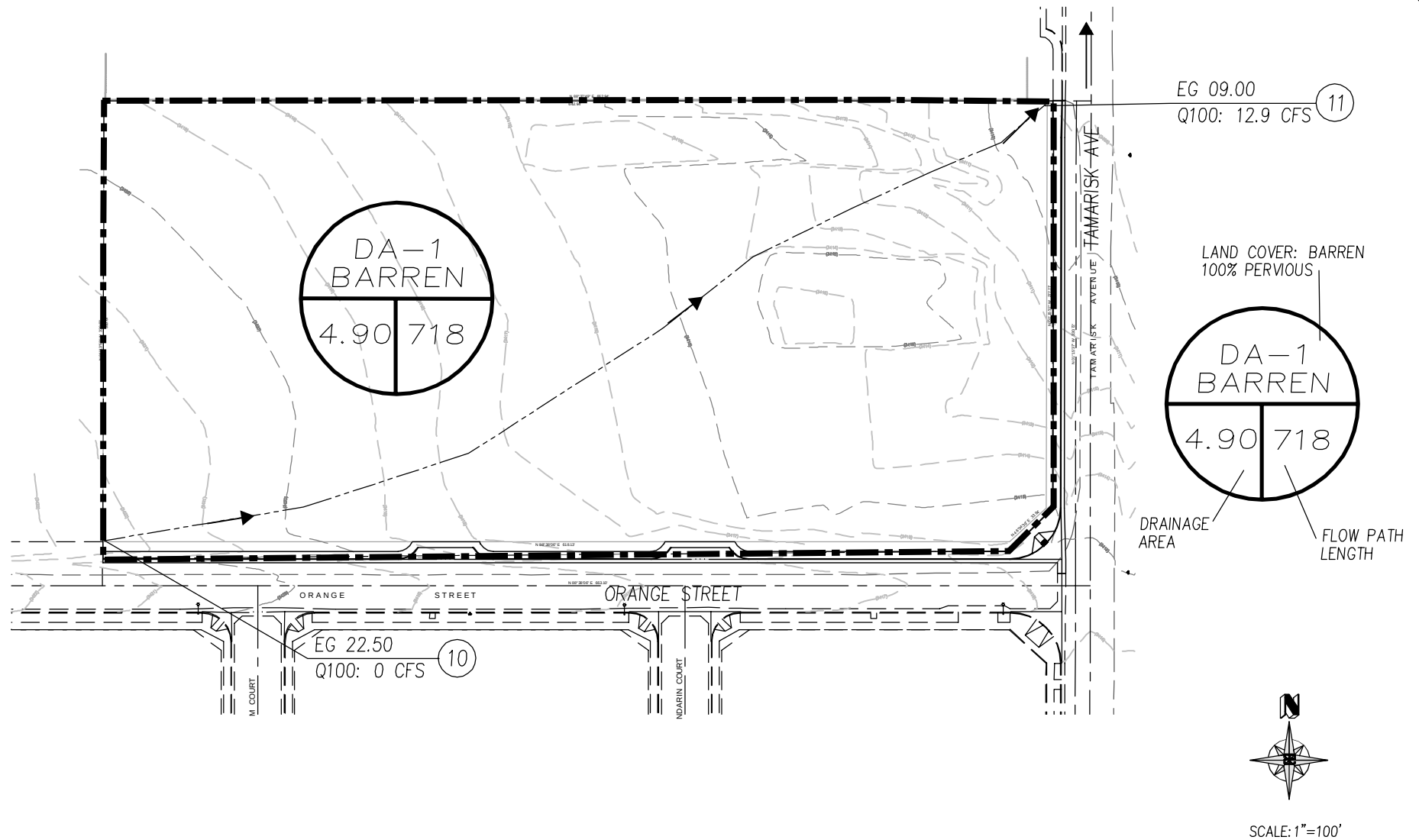
END OF STUDY SUMMARY:

TOTAL AREA(ACRES)	=	4.9	TC(MIN.) =	9.94
EFFECTIVE AREA(ACRES)	=	4.90	AREA-AVERAGED Fm(INCH/HR)=	0.16
AREA-AVERAGED Fp(INCH/HR)	=	0.74	AREA-AVERAGED Ap =	0.213
PEAK FLOW RATE(CFS)	=	18.55		

=====

END OF RATIONAL METHOD ANALYSIS

PLOT DATE: May 06, 2024 ashafiq



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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)
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Ver. 23.0 Release Date: 07/01/2016 License ID 1400

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* TAMARISK APARTMENT *
* HYDROLOGY ANALYSIS *
* 100YR STORM EVENT, PRE-DEVELOPED CONDITION *

FILE NAME: TAM.DAT
TIME/DATE OF STUDY: 15:57 05/06/2024

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 48.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL

SLOPE OF INTENSITY DURATION CURVE(LOG(I;IN/HR) vs. LOG(Tc;MIN)) = 0.7000
USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 1.2400

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB GUTTER-GEOMETRIES: HEIGHT (FT)	WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 718.00
ELEVATION DATA: UPSTREAM(FEET) = 22.50 DOWNSTREAM(FEET) = 9.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 16.135
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.110
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER "BARREN"	A	4.90	0.18	1.000	93	16.13

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.18
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000

```
SUBAREA RUNOFF(CFS) =      12.92
TOTAL AREA(ACRES) =      4.90   PEAK FLOW RATE(CFS) =      12.92
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES)      =      4.9   TC(MIN.) =      16.13
EFFECTIVE AREA(ACRES) =      4.90   AREA-AVERAGED Fm(INCH/HR)=  0.18
AREA-AVERAGED Fp(INCH/HR) =  0.18   AREA-AVERAGED Ap = 1.000
PEAK FLOW RATE(CFS)    =      12.92
=====
END OF RATIONAL METHOD ANALYSIS
```



ONSITE RETENTION VOLUME CALCULATION FOR HCOC MITIGATION

RETENTION VOL. REQUIRED TO MITIGATE HCOC CONDITION PER THE CITY
OF HESPERIA "13.5 CF/100 SF IMPERVIOUS AREA": 25,933 CF

RET/INFILTRATION CONTECH CHAMBER SYSTEM-1 CAPACITY: 16,642 CF
RET/INFILTRATION CONTECH CHAMBER SYSTEM-2 CAPACITY: 9,563 CF

TOTAL RET/INFILTRATION VOLUME PROVIDED: 26,205 CF > 25,933 CF

Target Captured Volume Watershed DMA 1

1) Calculate the "Watershed Imperviousness Ratio", I which is equal to the percent of impervious area in the BMP Drainage Area divided by 100

Imperviousness(i)= **0.9**

Total Acreage(A) = **4.90** 213444 sf

2) Calculate the composite Runoff Coefficient C_{bmp} for the drainage area

$$C_{bmp} = 0.858i^3 - 0.78i^2 + 0.774i + 0.04$$

C_{bmp} = **0.73**

3) Determine which Regression Coefficient to use by region the project is located in

Valley	1.481
Mountain	1.909
Desert	1.237

Regression coefficient for this project is: **1.481**

4) Determine the area averaged "6 hour Mean Storm Rainfall", P_6

2 yr 1 Hr Rainfall Depth per NOAA Atlas 14= **0.432** inches

P_6 = 2 yr 1 hr Rainfall x Regression coefficient

P_6 = **0.6398** inches

5) Determine Regression Constant (a) for 48 hour drawdown

a for 24 hour = 1.582
a for 48 hour = 1.963

a = **1.963**

6) Calculate the Maximized Detention Volume, P_0

$$P_0 = C \times a \times P_6$$

P_0 (inches) = **0.9172**

7) Calculate the Target Capture Volume, V_0 , in acre feet

$$V_0 = (P_0 \times A)/12$$

V_0 =

0.37 acre-feet

V_0 =

16,314 CF

REQD. WQ VOL.
: 16,314 CF

8) Retention Volume Calculation:

Use City rule of "13.5-cf of retention per 100-sf of impervious area"

***Retention Volume:**

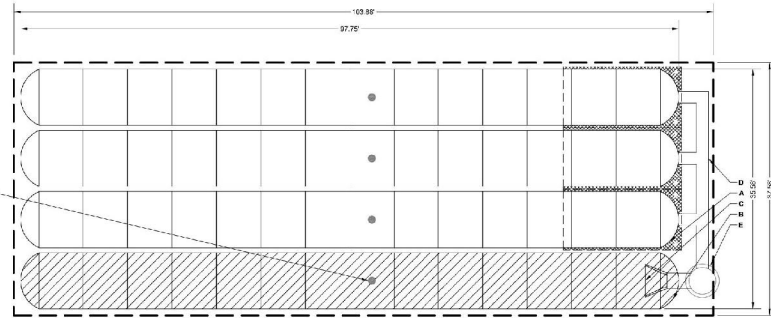
25,933 CF

$$[(4.9 \times 43560) \times 0.90] \times 13.5 / 100$$

***Required Retention Volume for HCOC mitigation.**

REQD. HCOC
MITIGATION VOL.:
25,933 CF

STORMTEC CHAMBER SYSTEM-1 CAPACITY CALC

[illegible]

 ISOLATOR ROW PLUS
(SEE DETAIL)

 PLACE MINIMUM 17.50' OF ADSP175 WOVEN GEOTEXTILE OVER BEDDING
STONE AND UNDERNEATH CHAMBER FEET FOR SCOUR PROTECTION AT ALL
CHAMBER INLETS (NOTES)

NOT

- NOTES**
- 1. MANHOLE SIZE IS TO BE DETERMINED BY GATE DESIGN ENGINEER. SEE TECH-NOTE BG-3 FOR MANHOLE SIZING GUIDANCE.
 - 2. DUE TO THE ADAPTATION OF THE CHAMBER DESIGN TO SPECIFIC SITE AND DESIGN CONDITIONS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANHOLE COMPONENTS IN THE FIELD.
 - 3. THE CHAMBER SHALL BE CONSTRUCTED TO BE ELEVATED AND, IF NECESSARY, ANCHOR GRADING TO EXCEED THE CHAMBER COVER REQUIREMENTS ARE MET.
 - 4. THE CHAMBER SHALL BE USED TO DISMISSE THE FLIGHT. SITE-SPECIFIC ORIGIN CRITERIA ON SOIL CONDITIONS OR AVOIDING CATASTROPHY. THIS SITE DESIGN ENGINEER IS RESPONSIBLE FOR THE SUFFICIENCY OF THE SOIL AND PROVIDING THE BEARING CAPACITY OF THE INSTALLED SOIL. THE BASE STONE DEPTH MAY BE INCREASED OR DECREASED UNLESS THIS INFORMATION IS PROVIDED.
- DO NOT FOR CONSTRUCTION:** THIS LAYOUT IS FOR DIMENSIONAL PURPOSES ONLY TO PROVIDE CONCEPT AS THE REQUIRED STORAGE VOLUME CAN BE ACHIEVED ON ANY PROPOSED SITE.

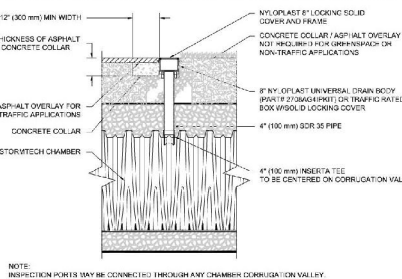
INSPECTION & MAINTENANCE

- STEP 1: INSPECT ISOLATOR ROOF PULP FOR SEDIMENT
- A. INSPECTION POINTS FOR PRESENT
- 1. REMOVED/CHIPPED LINER OR CRACKED/PEELING DRAIN
 - 2. REMOVED AND CLEAN FLEXPORT FILTER IF INSTALLED
 - 3. FILL IN A FLAME ARRESTOR OR FLEXPORT FILTER AT POINT OF SEDIMENT AND RECORD IN CHART
 - 4. LOCATE A CAMERA INTO DRAIN AND ROOF FOR VISUAL INSPECTION OF SEDIMENT (LEVELS) (SEE CHART FOR SEDIMENT BY LEVEL)
 - 5. RECORD IN CHART
- B. ALL SLOPE UP PULP
- 1. REMOVE COVER AND INSPECT LINE AT UPSTREAM END OF ISOLATOR ROOF PULP
 - 2. USE A FLAME ARRESTOR/INSPECT COVER (THE ISOLATOR ROOF PULP THROUGHOUT THE PULP LINE)
 - 3. MINORS OR NO SEDIMENT
 - 4. IF SEDIMENT OBSERVATION IS CONSIDERED, STOP INSPECTION, RETURN TO LINTING RANGE
 - 5. IF ISOLATOR ROOF, OR DRAINAGE, IS BEING MODIFIED TO STOP SEDIMENT, PROCEED TO STEP 2.
- STEP 2: CLEAN OUT ISOLATOR ROOF PULP USING THE JETTING PROCESS
- 1. CLEAN OUT DRAIN PULP USING THE JETTING PROCESS
 - 2. APPLY MAXIMUM PRESSURE OF 150 PSI AND INSURE DRAIN WATER IS OF 175°F OR MORE (SEE PREPARE)
 - 3. MAXIMUM STRUCTURE LIFE

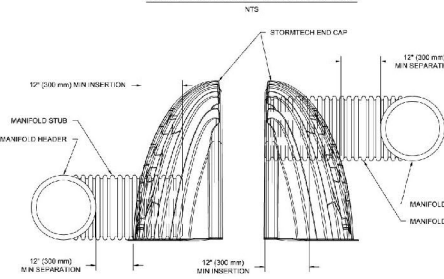
NOTES

1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ON ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

MC-7200 ISOLATOR ROW PLUS DETAIL



MC-SERIES END CAP INSERTION DETAIL



4	4" PVC INSPECTION PORT DETAIL (MC SERIES CHAMBER)
---	--

5	MC-SERIES END CAP INSERTION DETAIL
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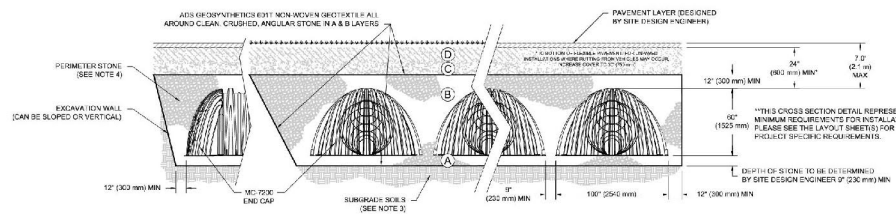
1 MC-7200 CROSS SECTION DETAIL

ACCEPTABLE FILL MATERIALS: STORMTECH MC-7200 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	ASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL MATERIAL FOR LAYER 12 STARTS FROM THE TOP OF THE C LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 12" LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS OR PER ENGINEERS PLANS CHECK FOR AND PER PAVEMENT SUBBASE PER 902, 903 AND 904	N/A	PREPARE PER SITE DESIGN ENGINEERS PLANS. PAVED INSTALLATIONS MAY HAVE STRONGER MATERIAL REQUIREMENTS (PER 904, 905 REQUIREMENTS)
	FINAL FILL FILL MATERIAL FOR LAYER 13 STARTS FROM THE TOP OF THE EMBEDEDMENT STONE (8" LAYER) TO 24" (600mm) ABOVE THE TOP OF THE CHAMBER, THE PAVEMENT SUBBASE MAY BE A PART OF THE 12" LAYER	GRANULAR WEL-GRANDED SUBGRADE MATERIALS - 30% FINES OR PROCESSED AGGREGATE JOINT PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYING	ASHTO M40 A-1, A-2, A-3 OR ASHTO M-31 3, 3.501, 4, 4.67, 5, 5.50, 5.7, 6, 6.7, 6.8, 7, 8, 8.9, 9, 10	BEGIN COMPACTIONS AT 24" (600mm) OF MATERIAL. COVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 2" (50mm) MAX. LIFT TO 4 MIN. 95% PRODUCTION DENSITY OR WEL-GRANDED MATERIAL AND 60% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.
B	EMBEDMENT STONE FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE (8" LAYER) TO THE C LAYER ABOVE	CLEAN CRUSHED, ANGULAR SILICEO OR RECYCLED CONCRETE	ASHTO M-31 3, 3.501, 4, 4.67, 5, 5.67	NO COMPACTION REQUIRED.
A	FOUNDATION STONE FILL 8" (200mm) DEEPER FROM THE SUBGRADE TO THE FOOT (BOTTOM) OF THE CHAMBER	CLEAN CRUSHED, ANGULAR STONE PER PROJECTS REQUIREMENTS	ASHTO M-31 3, 3.501, 4, 4.67, 5, 5.67	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE.

PLEASE NOTE

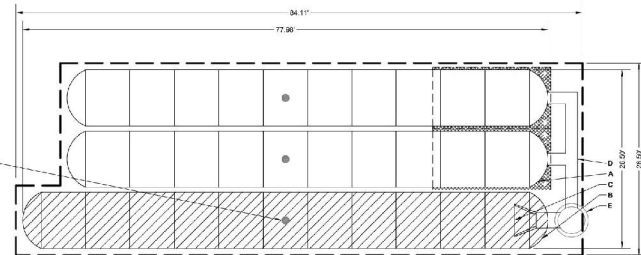
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NOTES

1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F4082, STANDARD SPECIFICATION FOR POLYETHYLENE (PE) CORRUGATED HDPE 18" (STANDARD) CORRUGATED CHAMBER/PIE CHAMBER CLASSIFICATION (SECTION 05120) CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2729 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC COLLAPSED WALL, STORMWATER COLLECTION CHAMBERS".
2. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
3. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
4. REINFORCEMENTS FOR MANHOLE AND INLET LIAISON:
- a. TO MAINTAIN THE STRENGTH OF CHAMBERS DURING SHIFTING AND HANDLING, CHAMBERS SHALL HAVE INTERNAL, INTERLOCKING STACKING LUGS.
 - b. TO ENSURE A SECURE JOINT DURING INSTALLATION AND SADDLE, THE HEIGHT OF THE CHAMBER JOINT MUST NOT BE LESS THAN 3".
 - c. TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, ALL OF THE ARCH 3 TOPPRESS CORNERS SHALL BE GREATER THAN OR EQUAL TO 40% RADIUS (R=10"). THE ARCH IS DEFINED IN SECTION 05120 OF ASTM F4082, AND c. TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 70° F / 21° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

STORMTEC CHAMBER SYSTEM-2 CAPACITY CALC

[illegible]

NOTE

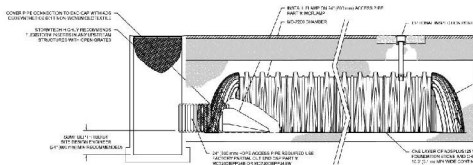
- MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER BASED ON TEST NOTE NO. 623 FOR MANIFOLD DISCHARGE CAPACITY. THE DISCHARGE CAPACITY OF THE CHAMBER COVER SHALL BE BASED ON THE DISCHARGE CAPACITY OF THE MANIFOLD. THE SITE DESIGN ENGINEER SHALL BE RESPONSIBLE FOR DETERMINING THE SUITABILITY OF THE SOIL AND PROVIDING THE BEARING CAPACITY OF THE INSTALLED SOILS. THE BASE COVER DEPTH MAY BE INCREASED OR DECREASED ONCE THIS INFORMATION IS OBTAINED.
- **NOT FOR CONSTRUCTION:** THIS LAYOUT IS FOR DIMENSIONAL PURPOSES ONLY TO PREPARE CONCEPT & THE REQUIRED STORAGE VOLUME CAN BE ACHIEVED ON SITE.

INSPECTION & MAINTENANCE

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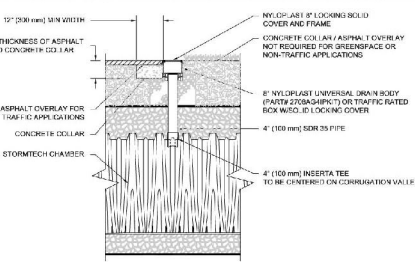
1

2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



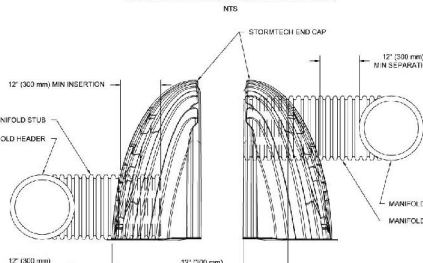
MC-7200 ISOLATOR ROW PLUG DETAIL

MC-7200 ISOLATOR ROW PLUS DETAIL



**4" PVC INSPECTION PORT DETAIL
(MC SERIES CHAMBER)**

MC-SERIES END CAP INSERTION DETAIL



NOTE: MANIFOLD STUD MUST BE LAID HORIZONTAL,
FOR A PROPER FIT IN END CAP OPENING.

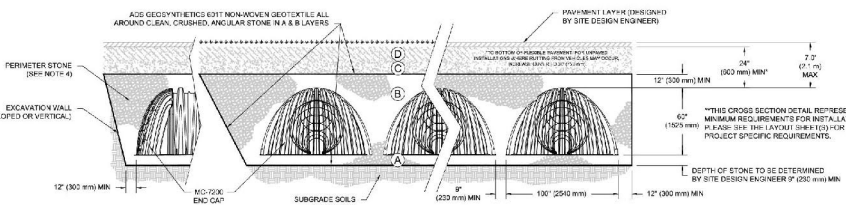
MC-SERIES END CAP INSERTION DETAIL

ACCEPTABLE FILL MATERIALS: STORMTECH MC-7200 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	ASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER D STARTS FROM THE TOP OF THE C LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT. OR UNPAVED / FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBGRADE MAY BE PART OF THE C LAYER	ANY SOURCE/CD MATERIALS IS, NATIVE SOILS OR PER HIGH ENGINEERING PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS	N/A	PREPARE PER SITE DESIGN ENGINEERING PLANS. PAVED INSTALLATIONS MAY HAVE VIBRATORY ROLLERS AND PREPARATION REQUIREMENTS
C	INITIAL FILL: FILL MATERIAL FOR LAYER C STARTS FROM THE TOP OF THE EMBANKMENT STONE (E LAYER) TO 24" (609 MM) ABOVE THE TOP OF THE CHASSIS. NOTE THAT PAVEMENT SUBGRADE MAY BE A PART OF THE C LAYER	GRANULAR WELLS GRADED SUBGRADE/AGGREGATE MATERIALS: 30% FINES OR PROCESSSED AGGREGATE. MOST PAVEMENT SUBGRADE MATERIALS CAN BE USED IN B.U. OF THIS LAYER.	ASHTO M101 A-1, A-2, A-3 OR ASHTO M33	NEED COMPACTIONS OF PER 24" (609 MM) OF MATERIAL. ONCE THE CHASSIS IS REACHED, COMPACT ADJACENT LAYERS IN 12" (305 MM) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR 100% GRADED MATERIALS AND 90% MAX LIFT DENSITY FOR PROCESSSED AGGREGATE MATERIALS.
B	EMBANKMENT STONE: FILL SURROUNDING THE CHASSIS FROM THE FOUNDATION STONE (A LAYER) TO THE C LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE	ASHTO M33 3, 394 / 4, 614 / 5, 36, 57	NO COMPACTION REQUIRED
A	FOUNDATION STONE: FILL BELOW CHASSIS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE C LAYER.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE	ASHTO M33 3, 397 / 4, 617 / 5, 56, 57	PLATE COMPACT (OR ROLL) TO ACHIEVE A FLAT SURFACE

PLEASE NOTE

- [illegible]



NOTES:

- C-CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F1518, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL, STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 200/151. 200/151 MEANS CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F1518/2779 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL, STORMWATER COLLECTION CHAMBERS".
- CHAMBERS SHALL BE DESIGNED TO PROVIDE A MINIMUM OF 10% BEARING CAPACITY FOR THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL HUMIDITY CONDITIONS.
4. PROPER STITCHING MUST BE EXTENDED TO THE INSTANTANEOUS YIELD POINT FOR BOTH VERTICAL AND SIDE TO SIDE EXCAVATION WALLS.
5. REQUIREMENTS FOR FOUNDATION AND INSTALLATION
- TO MAINTAIN THE CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LOGS.
 - TO MINIMIZE A SQUARE JOINT DURING INSTALLATION AND PACKING, THE WEIGHT OF THE CHAMBER JOINT MUST NOT BE LESS THAN 25 LBS.
 - THE WEIGHT OF THE INTERLOCKING INSTALLED CHAMBER JOINTS SHALL BE GREATER THAN OR EQUAL TO 40 LBS/FT². THE ASD IS DEFINED IN SECTION 6.2.2 OF ASTM F1518, AND TO RESIST C-CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 71° F/ 21° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLOR.

MC-7200 CROSS SECTION DETAIL